



MAX PLANCK INSTITUTE
FOR DYNAMICS OF COMPLEX
TECHNICAL SYSTEMS
MAGDEBURG



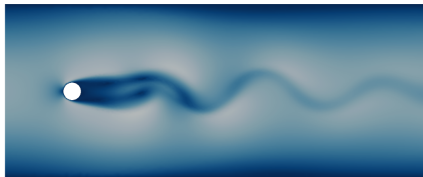
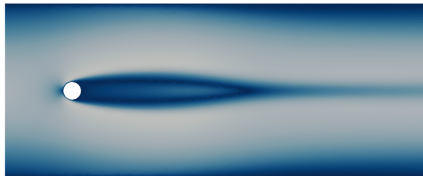
COMPUTATIONAL METHODS IN
SYSTEMS AND CONTROL THEORY

Robust control of incompressible flows

Peter Benner, Steffen W. R. Werner, Jan Heiland

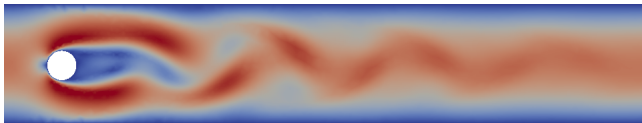
February 11th, 2020

Seminar talk at University of Deusto (CMC), Bilbao





1. Introduction
2. Uncertain Linearization Points are Coprime Factor Uncertainties
3. Robust Controller Design
4. Application to Incompressible Flows
5. Numerical Example
6. Conclusions
7. Misc and Bilbao

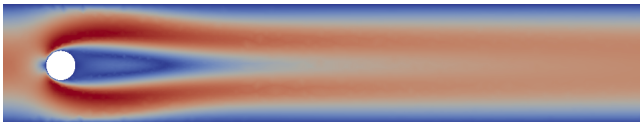


Feedback Control

Problem: The steady state is unstable: any perturbation – no matter how small – will trigger a transition into a periodic regime.

Goal: Stabilizing feedback controller that can handle:

- limited measurements,
- short evaluation time,
- system uncertainties.



Idea: Linearization-based feedback control for stabilization of the steady state.

[RAYMOND'05/'06, PB&JH'15, BREITEN&KUNISCH'14]

$$\begin{aligned}\dot{v} + (v \cdot \nabla)v - \nu \Delta v + \nabla p &= Bu, \\ \nabla \cdot v &= 0\end{aligned}$$

Linearization &
Semi-Discretization

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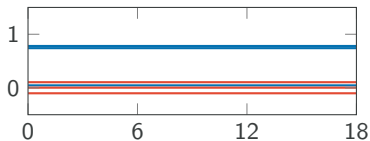
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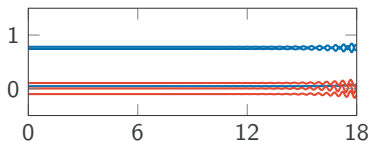
Fragility of Observer-Based Controllers

LQG controllers have no guaranteed robustness margins and will likely fail in the presence of system uncertainties.

LQG-feedback



corrupted LQG-feedback



In fact: [IEEE TRANSACTION ON AUTOMATIC CONTROL ('78)]:

Guaranteed Margins for LQG Regulators

JOHN C. DOYLE

Abstract—There are none.

Good news: Uncertainties that come from

- [CURTAIN'03]: Galerkin approximations of evolution systems,
- [PB&JH'17]: stable mixed-FEM approximation of the flow equations,
- [THIS TALK, PB&JH'16]: errors in the linearization point,

can be qualified as a coprime factor perturbation of the associated transfer function.

Even better news:

- [THIS TALK]: We can employ robust observer/controller design.



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Transfer functions

Mapping of inputs (controls) to outputs (measurements) in frequency domain, i.e., after Laplace transform of the system.

$$\begin{array}{l} \dot{x} = Ax + Bu \\ y = Cx \end{array} \quad \xrightarrow{\mathcal{L}(s)} \quad \begin{array}{l} sX(s) = AX(s) + BU(s) \\ Y(s) = CX(s) \end{array}$$

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- 2 But uncertainty in the operator gives another transfer function

$$G_{\Delta}(s) = C(sI - A - A_{\Delta})^{-1}B \in \mathbb{C}^{q,r}.$$

Coprime Factorization

Given a transfer function $G(s)$ of a linear system,

$$G(s) = M^{-1}(s)N(s)$$

is a **(left) coprime factorization** if there exist $X(s)$, $Y(s)$ such that the Bezout identity

$$M(s)X(s) + N(s)Y(s) = I$$

holds. Here, N , M , X , Y are all rational matrix functions with all poles in the open left half of the complex plane, i.e., they all represent stable linear systems.

Fact: N , M are coprime $\iff N$, M have no common zeros in the right half plane.

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Coprime Factor Perturbation

$$G_{\Delta}(s) = [N(s) + N_{\Delta}(s)][M(s) + M_{\Delta}(s)]^{-1}(s) \approx G(s) = N(s)M^{-1}(s),$$

where $N + N_{\Delta}$, $M + M_{\Delta}$ are stable.

Consider a state linear system (A, B, C) with

- $A: \mathcal{D}(A) \subset Z \rightarrow Z$ a generator of a C_0 -semigroup
- $B: U \rightarrow Z$ bounded and $C: Z \rightarrow Y$ bounded
- U, Y, Z Hilbert spaces, U, Y finite dimensional

and

$$(A_\Delta, B, C) \sim G_\Delta \approx G \sim (A, B, C)$$

with a certain difference in the dynamics which is caused, say, by an inexact linearization.

Theorem (PB&JH '16)

If (A_Δ, B, C) and (A, B, C) are jointly stabilizable (or detectable), i.e., there exists a **state** feedback K (or L) that stabilizes (or makes detectable) both (A_Δ, B, C) (or (A, B, C))¹, then G differs from G_Δ through a coprime factor perturbation

$$\Delta = \begin{bmatrix} M_\Delta & N_\Delta \end{bmatrix}$$

with $\|\Delta\|_\infty \rightarrow 0$ as $A \rightarrow A_\Delta$ in the operator norm.

¹That is, $A + BK$ and $A_\Delta + BK$ or $A + LC$ and $A_\Delta + LC$ are all stable.



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Robust controllers for coprime factor uncertainty

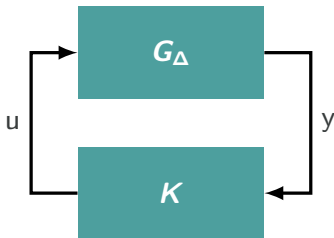
An admissible controller K stabilizes

$$G_{\Delta} = (M + M_{\Delta})^{-1}(N + N_{\Delta})$$

for all $\|\Delta\|_{\infty} = \|[M_{\Delta} \ N_{\Delta}]\|_{\infty} < \epsilon$,

if and only if²

- K stabilizes $G = M^{-1}N$ and
- $\left\| \begin{bmatrix} K \\ I \end{bmatrix} (I - GK)^{-1} M^{-1} \right\|_{\infty} \leq \epsilon^{-1}$.



Design of robust controllers

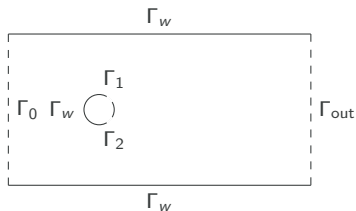
In finite dimensions, the Riccati based \mathcal{H}_{∞} -controller with parameter γ is robustly stabilizing with $\epsilon = \gamma^{-1}$; see Cor. 3.9 in [MCFARLANE&GLOVER'90].

²See, e.g. [MCFARLANE&GLOVER'90] for the finite dimensional case and [CURTAIN&ZWART'95] for the infinite dimensional case



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We consider



where

- V ... velocity,
- P ... pressure,
- ν ... diffusion parameter,

$$\dot{V} + (V \cdot \nabla)V + \nabla P - \nu \Delta V = 0,$$

$$\operatorname{div} V = 0, \quad \text{in } \Omega,$$

$$\nu \frac{\partial V}{\partial n} - nP = 0 \text{ on } \Gamma_{out},$$

$$V = 0 \text{ on } \Gamma_w,$$

$$V = ng_0 \cdot \alpha \text{ on } \Gamma_0,$$

$$V = ng_1 \cdot u_1 \text{ on } \Gamma_1,$$

$$V = ng_2 \cdot u_2 \text{ on } \Gamma_2,$$

- g_0, g_1, g_2 ... spatial shape functions,
- u_1, u_2 ... scalar input functions,
- α ... magnitude of the inflow velocity,
- n ... normal vector at the boundaries.

To design a controller, we proceed as follows

- 1 We relax the Dirichlet control $V|_{\Gamma_1} = g_1 u - \varepsilon(\nu \frac{\partial V}{\partial n} - Pn)$
- 2 Let v_α be the steady state solution for zero inputs, and let $v_\delta(t) = V(t) - v_\alpha$ the deviation.
- 3 We consider the linearization

$$\dot{v}_\delta + (v_\delta \cdot \nabla)v_\alpha + (v_\alpha \cdot \nabla)v_\delta + \nabla p_\delta - \nu \Delta v_\delta = 0$$

that is a valid approximation as long as v_δ is small.

$$\begin{aligned} \dot{v}_\delta + (v_\delta \cdot \nabla)v_\alpha + (v_\alpha \cdot \nabla)v_\delta + \nabla p_\delta - \nu \Delta v_\delta &= 0 \\ \operatorname{div} v_\delta &= 0 \end{aligned}$$

Then, with

$$\mathcal{H}_{div} := \{v \in L^2(\Omega) : \operatorname{div} v = 0, v \cdot n = 0 \text{ on } \Gamma_w \cap \Gamma_{out}\}$$

as the state space, the (orthogonal) *Leray*-projector

$$\Pi \in \mathcal{L}(L^2(\Omega)): L^2(\Omega) \mapsto \mathcal{H}_{div},$$

and $x := \Pi v_\delta$ the model reads³

$$\begin{aligned} \dot{x} &= A_\alpha x + \Pi B u \quad \text{in } \mathcal{H}_{div}, \\ y &= C x \end{aligned}$$

where

- $A_\alpha: \mathcal{D}(A_\alpha) \subset \mathcal{H}_{div} \rightarrow \mathcal{H}_{div}$ is the *Oseen* operator
- $\Pi B: \mathbb{R}^2 \rightarrow \mathcal{H}_{div}$ is the input operator
- $C: \mathcal{H}_{div} \rightarrow \mathbb{R}^q$ is the output operator

³The pressure p_δ is gone, since Π maps along the orthogonal complement of the gradient



- ✓ The linearized model is a standard (A, B, C) system
 - we know: A_α is the generator of a C_0 -semi group [RAYMOND'06]
 - we choose: C to be bounded
 - we show below: ΠB is bounded.
- The theory for robust stabilization of linearization errors applies.

As for the input on Γ_1 (and similarly for Γ_2):

- The input operator is defined via

$$\langle B_1 u, w \rangle = -\frac{1}{\varepsilon} \int_{\Gamma_1} n g_1 w \, ds \cdot u, \quad w \in \mathcal{H}_{div},$$

- as it comes from the integration by parts of $\langle -\nu \Delta V + \nabla P, w \rangle$
- and the definition of the Robin conditions.

✓ This operator is bounded as a map $B_1: \mathbb{R} \rightarrow \mathcal{H}_{div}$, since:

- $\sup_{u \in \mathbb{R}, |u|=1} \|B_1 u\|_{X^*} < \infty$ if $\sup_{w \in X, \|w\|=1} \left| \frac{1}{\varepsilon} \int_{\Gamma_1} n g_1 w \, ds \right| < \infty$,
- the *trace operator* $w \mapsto n w|_{\Gamma_1}$ is bounded for $X = \mathcal{H}_{div}$,
- and since \mathcal{H}_{div} is a closed subspace of $L^2(\Omega)$ so that $\mathcal{H}_{div} \simeq (\mathcal{H}_{div})^*$,

→ provided that the shape function g_1 is sufficiently smooth.

- Interestingly, $B: U \rightarrow L^2(\Omega)$ is not bounded, but $\Pi B: U \rightarrow L^2(\Omega)$ is.



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6. Conclusions
7. Misc and Bilbao

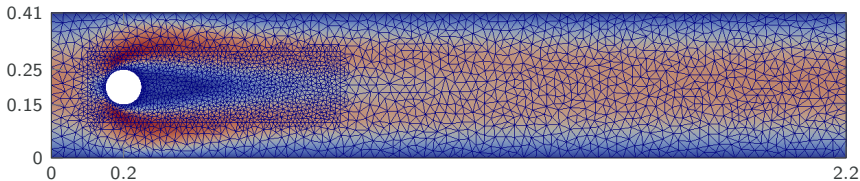


Fig.: 2D cylinder wake, discretized by Taylor-Hood (P_2/P_1) finite elements.

- Navier-Stokes equation
- Reynolds 90
- 9,843 velocity nodes
- distributed observations:
 - 3 sensors in the wake
 - measuring both v components

Target

Stabilize the steady-state and compensate perturbations to suppress vortex shedding.

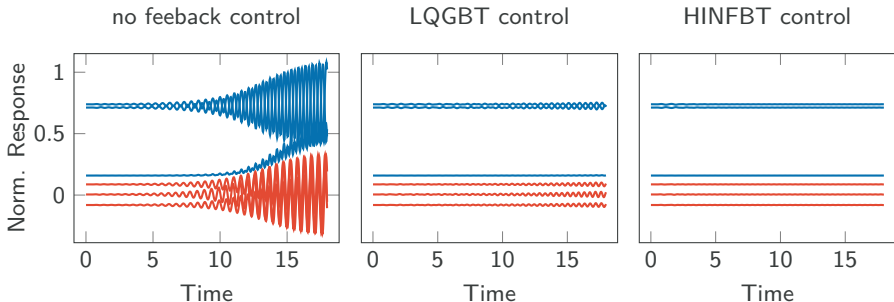
- boundary control:
 - 2 outlets at the cylinder periphery
 - control by injection and suction



ℓ	$\frac{\ v_\infty - v_\ell\ }{\ v_\infty\ }$	$\ \Delta_\ell\ _{\mathcal{H}_\infty}$	γ_ℓ^{-1}
3	0.094	2.323	0.103
5	0.030	0.579	0.204
6	0.018	0.168	0.233
7	0.011	0.226	0.237
8	0.006	0.123	0.240
10	0.002	0.028	0.242

Test setup:

- v_∞ the (exact) steady state
- $v_\ell \approx v_\infty$ computed by ℓ *Picard* steps starting from the Stokes-solution
- $A := A(v_\infty)$ the exact linearization
- $A + A_\Delta := A_\ell$ the inexact linearization about v_ℓ
- Δ_ℓ the difference in the coprime factorizations
- see [PB&JH&SW'19] for how to compute the norms.



- error in linearization: 8%
- reduced-order controller dimension: 7
- trigger of instabilities by input disturbance on time interval $[0, 1]$:

$$u_{\delta}(t) = \begin{bmatrix} 0.01 \sin(2t\pi) \\ -0.01 \sin(2t\pi) \end{bmatrix}$$



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Summary

Robust controller

- that compensate linearization errors
- can be analysed via coprime factorizations and
- can be designed with Riccati-based \mathcal{H}_∞ -theory.

The general ∞ -dimensional theory

- applies to control of incompressible flows
- if Dirichlet control is relaxed as Robin control.

In finite dimensional simulations, we can

- compute the errors in the factorization
- and provide controller with guaranteed robustness.

Outlook

- Quantify the error in the factorizations.
- Incorporate the discretization error in the controller design.

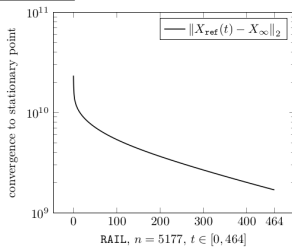
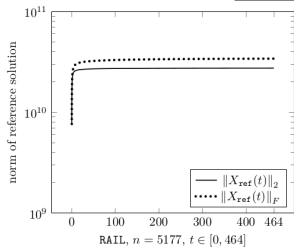


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- We design feedback controls:

$$u = -B^* Xx \tag{1}$$

- For the presented stabilization we base on the steady state Riccati solution X_∞ .
- For finite time horizons we would consider the differential Riccati equation
- Well known and well observed $X(t) \rightarrow X_\infty$ as $t \rightarrow \infty$ (turnpike)
- My plan for Bilbao:
 - Theory – combine the Riccati results and turn pike results.
 - Practice: exploit the turnpike for efficient solvers for the differential Riccati equation.





P. Benner and J. Heiland.

LQG-balanced truncation low-order controller for stabilization of laminar flows. In R. King, editor, *Active Flow and Combustion Control 2014*, volume 127 of *Notes on Numerical Fluid Mechanics and Multidisciplinary Design*, pages 365–379. Springer International Publishing, 2015.



P. Benner and J. Heiland.

Robust stabilization of laminar flows in varying flow regimes. *IFAC-PapersOnLine*, 49(8):31–36, 2016.
2nd IFAC Workshop on Control of Systems Governed by Partial Differential Equations CPDE 2016, Bertinoro, Italy, 13–15 June 2016.



P. Benner and J. Heiland.

Convergence of approximations to Riccati-based boundary-feedback stabilization of laminar flows. *IFAC-PapersOnLine*, 50(1):12296–12300, 2017.
20th IFAC World Congress.



P. Benner, J. Heiland, and S. W. R. Werner.

Robust controller versus numerical model uncertainties for stabilization of Navier-Stokes equations.

In 3rd IFAC Workshop on Control of Systems Governed by Partial Differential Equations, 2019.



T. Breiten and K. Kunisch.

Riccati-based feedback control of the monodomain equations with the Fitzhugh–Nagumo model.

SIAM J. Control Optim., 52(6):4057–4081, 2014.



R. F. Curtain.

Model reduction for control design for distributed parameter systems.

In R. Smith and M. Demetriou, editors, Research Directions in Distributed Parameter Systems, pages 95–121. SIAM, Philadelphia, PA, 2003.



R. F. Curtain and H. Zwart.

An Introduction to Infinite-Dimensional Linear Systems Theory, volume 21 of *Texts in Applied Mathematics*.

Springer-Verlag, New York, 1995.



D. C. McFarlane and K. Glover.

Robust Controller Design Using Normalized Coprime Factor Plant Descriptions,
volume 138.

Springer, 1990.



J.-P. Raymond.

Local boundary feedback stabilization of the Navier-Stokes equations.

In *Control Systems: Theory, Numerics and Applications, Rome, 30 March – 1 April 2005*, Proceedings of Science. SISSA, 2005.

Available from <http://pos.sissa.it>.



J.-P. Raymond.

Feedback boundary stabilization of the two-dimensional Navier-Stokes equations.

SIAM J. Control Optim., 45(3):790–828, 2006.